

# ON PLANE FLOWS OF AN INCOMPRESSIBLE FLUID OF VARIABLE VISCOSITY

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## ABSTRACT

In this paper, we indicate that the equations governing the motion of an incompressible fluid of variable viscosity for an arbitrary state equation possess an infinite set of solutions for the flows characterized by the equation  $y = R(x) + C_1\Psi + C_2$  where  $\Psi$  is the streamfunction and  $R(x)$  the arbitrary function. The streamline patterns for the flows in unbounded and bounded domains are also presented for some forms of the function  $R(x)$ .

**Key words:** Incompressible fluid of variable viscosity, plane flows, a class of plane flows, plane flows using von-Mises coordinates.

## 1. INTRODUCTION

The objective of this paper is to indicate that the equations describing the motion of an incompressible fluid of variable viscosity possess an infinite set of solutions for the flows characterized by the equation  $y = R(x) + C_1\Psi + C_2$  where  $\Psi$  is the streamfunction,  $R(x)$  is the arbitrary function, and  $C_1 (\neq 0)$  and  $C_2$  are arbitrary constants. To achieve our objective, we treat  $x$  and  $\Psi$  as the independent variables and recast the flow equations in the von-Mises coordinates system  $(x, \Psi)$ . von-Mises coordinates are used by many researchers [1-4] to obtain the numerical solutions of the flow equations for inviscid fluids. The paper is organized in the following fashion: In section (2), we transform the flow equations in the von-Mises system  $(x, \Psi)$ . In section (3), we determine the exact solutions of the flow equations using the method of differentiation and integration [5,6] and present flow patterns for some forms of the function  $R(x)$  in unbounded domains and boundary value problems.

## 2. BASIC FLOW EQUATIONS

The non-dimensional equations describing the steady plane motion of an incompressible fluid of variable viscosity  $\mu$  and constant thermal conductivity  $k$  are [7]

$$u_x + v_y = 0 \quad (1)$$

$$u u_x + v u_y = -p_x + [(2\mu u_x)_x + (\mu\{u_y + v_x\})_y] / \text{Re} \quad (2)$$

$$u v_x + v v_y = -p_y + [(2\mu v_y)_y + (\mu\{u_y + v_x\})_x] / \text{Re} \quad (3)$$

$$u T_x + v T_y = [T_{xx} + T_{yy}] / \text{Re Pr} + \text{Ec} [2\mu(u_x^2 + v_y^2) + \mu(v_x + u_y)^2] / \text{Re} \quad (4)$$

The meaning of various symbols used here are given in nomenclature. On introducing the vorticity  $\omega$  and the total energy function  $L$  defined by:

$$\omega = v_x - u_y \quad (5)$$

$$L = p + (u^2 + v^2) / 2 - 2\mu u_x / \text{Re} \quad (6)$$

the equations (1-4) can be rewritten as:

$$u_x + v_y = 0 \quad (7)$$

$$-v\omega = -L_x + [\mu\{u_y + v_x\}]_y / \text{Re} \quad (8)$$

$$u\omega = -L_y + [-(4\mu u_x)_y + (\mu\{u_y + v_x\})_x] / \text{Re} \quad (9)$$

$$u T_x + v T_y = [T_{xx} + T_{yy}] / \text{Re Pr} + \text{Ec} [2\mu(u_x^2 + v_y^2) + \mu(v_x + u_y)^2] / \text{Re} \quad (10)$$

In von-Mises coordinates  $(x, \Psi)$ , the velocity components  $u, v$  and partial derivatives  $(\cdot)_x, (\cdot)_y$  are given by

$$u = 1/y_\Psi, \quad v = y_x/y_\Psi \quad (11)$$

$$\begin{aligned} (\cdot)_x &= (\cdot)_x + (y_x/y_\Psi)(\cdot)_\Psi \\ (\cdot)_y &= (1/y_\Psi)(\cdot)_\Psi \end{aligned} \quad (12)$$

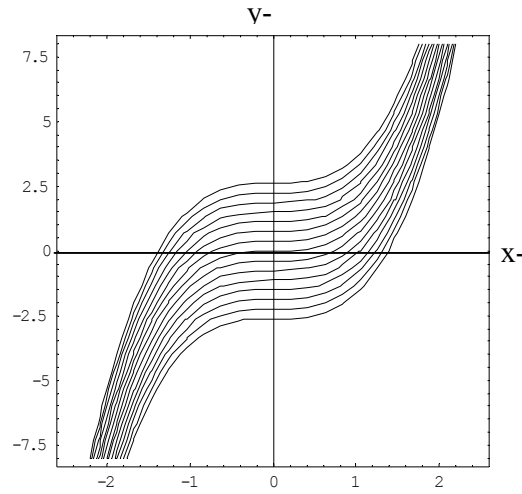
where in above “ $\cdot$ ” denotes any function. Equations (7-10), using Eqs. (11), (12), and  $y = R(x) + C_1\Psi + C_2$ , are replaced by

$$R'' = -C_1 L_\Psi - R' R'' \mu_\Psi / \text{Re} + C_1 (\mu R'' )_x / \text{Re} \quad (13)$$

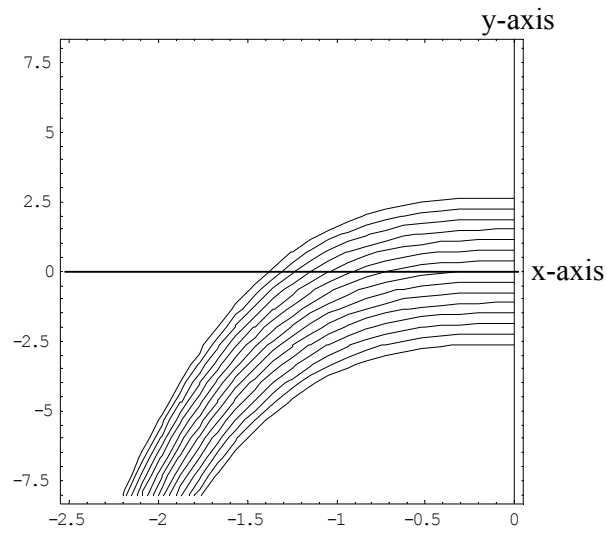
$$-C_1 L_x + R' (\mu R'' )_x / \text{Re} + (1 + R'^2) R'' \mu_\Psi / C_1 \text{Re} = 0 \quad (14)$$

$$\begin{aligned} T_{xx} - R'' T_\Psi / C_1 - 2R' T_{x\Psi} / C_1 \\ + (1 + R'^2) T_{\Psi\Psi} / C_1^2 - \text{Re Pr} T_x / C_1 \\ = -\text{Ec Pr} \mu R''^2 / C_1^2 \end{aligned} \quad (15)$$

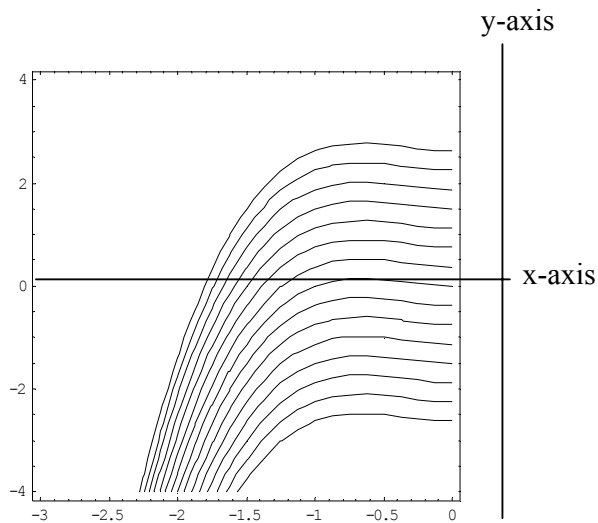
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**Figure – 1: Streamline pattern for  $y-x^3=\text{constant}$  (unbounded domain)**



**Figure – 2: Streamline pattern for  $y-x^3=\text{constant}$  for boundary value problem**



**Figure-3: Streamlines pattern for  $y-x^3-x^2=\text{constant}$  (unbounded domain)**

**3. SOLUTIONS**

In this section we determine some solutions of the system of equations (13-15).

Equations (13) and (14), on using the integrability condition

$$L_{xy} = L_{yx}, \text{ yield}$$

$$R'' \mu_{xx} - 2 R' R'' \mu_{x\psi} / C_1 + 2 R''' \mu_x - [(R' R'')_x + R' R'''] \mu_\psi / C_1 - R'' (1 + R'^2) \mu_{\psi\psi} / C_1^2 + R^{IV} \mu = Re R''' / C_1 \quad (16)$$

Equation(16) is the equation which the function R(x) and viscosity  $\mu$  must satisfy for the flows characterized by Eq.(11). Once a solution of this is determined, the function L and temperature T are determined from Eqs.(13–15). If we treat Eq.(16) as a partial differential equation in  $\mu$  the coefficients suggests to assume  $\mu$  of the form

$$\mu = M(x) + M_1(x) v \quad (17)$$

Equation (16), on utilizing Eq.(17), becomes

$$R'' [M'' + M_1'' v(\psi)] - 2 R' R'' M_1' + 2 R''' [M' + M_1' v(\psi)] - [(R' R'')_x + R' R'''] M_1 / C_1 + R^{IV} (M + M_1 v(\psi)) = Re R''' / C_1 \quad (18)$$

where

$$v(\psi) = C_1 \psi + C_2$$

Since x and  $\psi$  are independent variables, therefore, Eq.(18) holds for all x and  $\psi$  provided:

$$R'' M_1'' + 2 R''' M_1' + R^{IV} M_1 = 0 \quad (19)$$

and

$$R'' M'' - 2 R' R'' M' + 2 R''' M - [(R' R'')_x + R' R'''] M_1 / C_1 + R^{IV} M = Re R''' / C_1 \quad (20)$$

The solution of Eq.(19), for  $R'' \neq 0$ , is

$$M_1 = (C_3 x + C_4) / R'' \quad (21)$$

where  $C_3 (\neq 0)$  and  $C_4$  are arbitrary constants

Substituting Eq.(21) in Eq.(20) and integrating twice the resulting equation, we obtain:

$$M(x) = (\int [\int N(x) dx + C_5] dx + C_6) / R'' \quad (22)$$

where

$$N(x) = Re R''' / C_1 + 2 R' R'' M_1' + [(R' R'')_x + R' R'''] M_1 / C_1 \quad (23)$$

and  $C_5, C_6$  are arbitrary constants. Since in Eqs.(21) and (22), the function R(x) is arbitrary, we can generate a large number of expressions for viscosity  $\mu$ .

The temperature Eq.(15), for viscosity  $\mu$  defined in Eq.(17), becomes

$$T_{xx} - Re Pr T_x / C_1 - 2 R' T_{x\psi} / C_1 - R'' T_\psi / C_1 + (1 + R'^2) T_{\psi\psi} / C_1^2 = - Ec Pr R''^2 (M + M_1 v) / C_1^2 \quad (24)$$

We seek a solution of Eq. (24) of the form

$$T = T_1(x) + T_2(x) v + T_3(x) v^2 + \zeta(v) \quad (25)$$

Eq.(15), on using Eq.(25), yields

$$N_1(x) + N_2(x) v + N_3(x) v^2 + (1 + R'^2) \zeta'' - R' \zeta' = 0 \quad (26)$$

where the functions  $N_1(x), N_2(x), N_3(x)$  are given in appendix A.

Differentiating Eq.(26) w. r. t 'v', we get:

$$N_2 + 2 N_3 v + (1 + R'^2) \zeta''' - R'' \zeta'' = 0 \quad (27)$$

Differentiating Eq.(27) w. r. t 'v', we get:

$$2 N_3 + (1 + R'^2) \zeta^{IV} - R''' \zeta''' = 0 \quad (28)$$

Differentiating Eq.(28) w. r. t 'v', we obtain:

$$(1 + R'^2) \zeta^V / R'' - \zeta^{IV} = 0 \quad (29)$$

On differentiating Eq.(29) w. r. t 'x', we get:

$$[(1 + R'^2) / R'']' \zeta^V = 0 \quad (30)$$

This holds for all x and v( $\psi$ ) provided:

$$(i) \zeta^V = 0, [(1 + R'^2) / R'']' \neq 0.$$

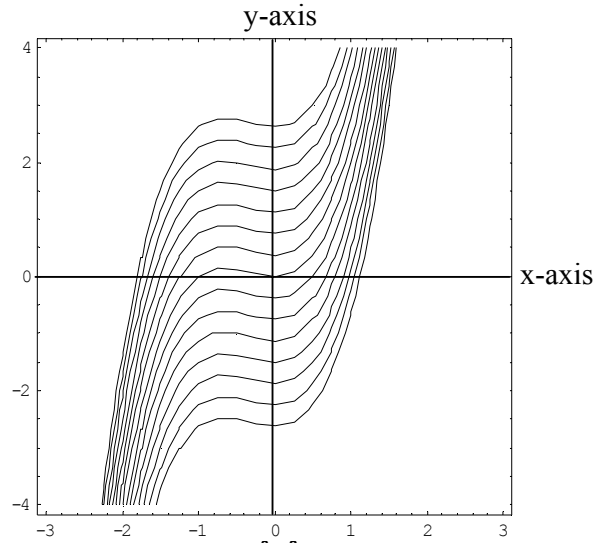


Figure-4: Streamlines pattern for  $y-x^3-x^2 = \text{constant}$  for boundary value problem

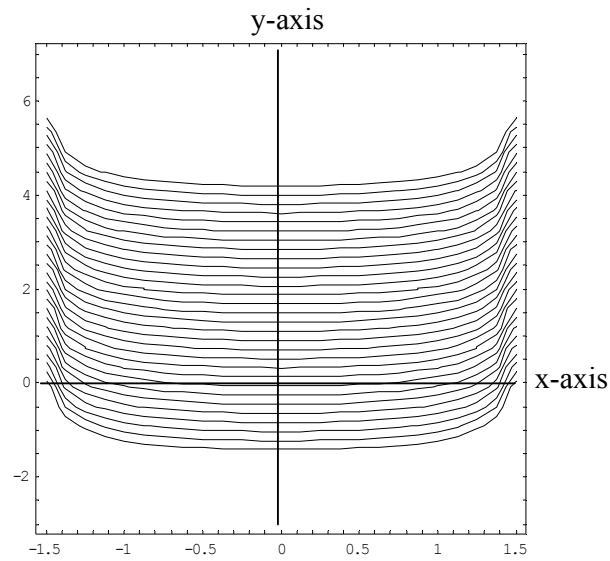


Figure-5: Streamlines pattern for  $y - \log[\text{Sec}x + 3] = \text{constant}$  for unbounded domain

(ii)  $[(1 + R'^2)/R'']' = 0, \zeta^V \neq 0.$

We consider these two cases separately.

Case (i) When  $\zeta^V = 0$ , we get

$$\zeta(v) = \frac{C_7 v^4}{10 v} + \frac{C_8 v^3}{6} + \frac{C_9 v^2}{2} + C_{10} v + C_{11} \quad (31)$$

where  $C_7, C_8, C_9, C_{10}, C_{11}$  are constants. Substituting Eq. (31) in Eq.(29), we get

$$C_7 = 0 \quad (32)$$

Equations (32) and (28), yield

$$2 N_3 - R'' C_8 = 0 \quad (33)$$

The solution of Eq (33), utilizing the expression for  $N_3(x)$ , is

$$T_3 = \int (C_8 R' / 2 + C_{12}) \exp(-Re Pr x / C_1) dx + C_{13} \exp(Re Pr x / C_1) \quad (34)$$

where  $C_{12}, C_{13}$ , are non-zero arbitrary constants.

Equation (27), on using Eqs. (31-33), yields

$$N_2 = C_9 R'' - C_8 (1 + R'^2) \quad (35)$$

On substituting expression for  $N_2(x)$  in Eq. (35) and integrating twice the resulting differential equation, we get

$$T_2 = \int \exp(-Re Pr x / C_1) \int \exp(-Re Pr x / C_1) N_4(x) dx + C_{14} dx + C_{15} \quad (36)$$

where

$$N_4(x) = C_9 R'' - C_8 (1 + R'^2) + 2 R'' T_3 + 4 R' T_{3x} - Ec Pr R''^2 M_1 / C_1^2 \quad (37)$$

Finally, utilizing the above results in Eq.(26) and the expression for  $N_1(x)$ , we obtain

$$T_1 = \int \exp(-Re Pr x / C_1) \int N_5 \exp(-Re Pr x / C_1) dx + C_{16} dx + C_{17} \quad (38)$$

where

$$N_{5} = C_{10} R'' - C_9 (1 + R'^2) + R'' T_2 / C_1 + 2 R' T_{2x}$$

$$- 2 (1 + R'^2) T_3 - Ec Pr R''^2 M / C_1^2 \quad (39)$$

We note that the function  $R(x)$  is still arbitrary and, therefore, we can construct a large number of solutions to the flow equations. In Eqs.(36-38),  $C_{14}, C_{15}, C_{16}, C_{17}$  are all non-zero arbitrary constants.

Case (ii) When  $[(1 + R'^2)/R'']' = 0$ , then

$$R = [\ln \sec(x / C_{18} + C_{19})] / C_{18} + C_{20} \quad (40)$$

where  $C_{18} (\neq 0), C_{19}, C_{20}$  are arbitrary constants.

The expression for the function  $R$  must satisfy the Eq. (29) and therefore we get:

$$C_{18} \zeta^V - \zeta^{IV} = 0 \quad (41)$$

The solution of Eq.(41) is:

$$\zeta = \exp(v / C_{18}) \{ [C_{21} v^3 / 6 + C_{22} v^2 / 2 + C_{23} v + C_{24}] \exp(-v / C_{18}) + C_{25} \} \quad (42)$$

where  $C_{21}, C_{22}, C_{23}, C_{24}, C_{25}$  are all non-zero constants.

Equation (28), utilizing Eqs.(40) and (41), yields

$$N_3 = -C_{21} C_{18} R'' / 2 \quad (43)$$

Equation (27),employing Eqs.(40-43), yields

$$N_2 = -C_{22} C_{18} R'' \quad (44)$$

Substituting the expressions of  $\zeta(\Psi), N_2, N_3$  in Eq.(26), we get:

$$N_1 = -C_{18} C_{23} R'' \quad (45)$$

On using the definitions of  $N_1, N_2, N_3$  from appendix A and after integration, we obtain

$$T_1 = Z_3 \int [Z_3^{-1} \{ \int Z_2 dx + C_{31} \} dx] + C_{32} Z_3 \quad (46)$$

$$T_2 = Z_3 \int [Z_3^{-1} \{ \int Z_1 dx + C_{29} \} dx] + C_{30} \quad (47)$$

$$T_3 = -C_{21} C_{18} \int [Z_3 \{ \int R' Z_3^{-1} dx \} dx] / 2 - C_{18}^2 C_{26} Z_3 / Re^2 Pr^2 + C_{18} C_{27} Z_3 / Re Pr + C_{28} \quad (48)$$

In Eqs.(46-47),  $Z_1 = -C_{18} C_{22} R'' + 2 R'' T_3 + 4 R' T_{3x}$

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$$-Ec Pr R'' M_1(x) / C_1^2 \quad (49)$$

$$Z_2 = -C_{18} C_{23} R'' + R'' T_2 / C_1 + 2 R' T_{2x} / C_1^2 - 2(1 + R'^2) T_3 - Ec Pr R''^2 M(x) / C_1^2 \quad (50)$$

$$Z_3 = \exp(Re Pr x / C_1) \quad (51)$$

The solution of Eq.(16) can further be extended by assuming:

$$\mu = M(x) + M_1(x)v + M_2(x)v^2 \quad (52)$$

Substituting Eq.(52) in Eq.(16), we get:

$$X_1(x) + X_2(x)v + X_3(x)v^2 = 0 \quad (53)$$

where the functions  $X_1(x), X_2(x), X_3(x)$ , are given in appendix A.

The solution of Eq.(53), following the same procedure as that of Eq.(18), is given by:

$$M_2 = (a_1 x + a_2) / R'' \quad , R'' \neq 0 \quad (54)$$

$$M_1 = \left\{ \int \left[ \int L_1(x) dx + a_3 \right] dx + a_4 \right\} / R'' \quad (55)$$

$$M = \left\{ \int \left[ \int L_2(x) dx + a_3 \right] dx + a_5 \right\} / R'' \quad (56)$$

where

$$L_1(x) = 4 R' R'' M_2' + 2 [(R' R'')_x + (R' R''')] M_2 \quad (57)$$

$$L_2(x) = 2 R' R'' M_1' + [(R' R'')_x + R' R'''] M_1 + 2 R'' (1 + R'^2) M_2 + Re R'' / C_1 \quad (58)$$

and  $a_1, a_2, a_3, a_4, a_5$  are all non-zero arbitrary constants. We note that the function  $R(x)$  in Eq.( 54– 56) is arbitrary and therefore we can construct a large number of expressions for viscosity  $\mu$  and the velocity components  $u, v$ .

The form for  $\mu$  in Eq. (52), suggests to seek a solution of Eq.(15) in the form:

$$T = T_1(x) + T_2(x)v + T_3(x)v^2 + T_4(x)v^3 + \zeta(v) \quad (59)$$

This, on substituting in Eq.(15), we obtain:

$$N_6(x) + N_7(x)v + N_8(x)v^2 + N_9(x)v^3 + (1 + R'^2)\zeta'' - R''\zeta' = 0 \quad (60)$$

where  $N_6(x), N_7(x), N_8(x), N_9(x)$  are given in appendix B.

The solution of Eq.(60) can easily be determined in the same manner as that of Eq.(26). We mention that the function  $R(x)$  in the solution of Eq.(60) also remains arbitrary, and, therefore, we can construct a large number of solutions to the flow equations.

Finally, for the sake of completeness, we consider some forms of the function  $R(x)$  and the boundary value problems. When  $R(x) = x^3$ , the flow pattern in unbounded domain is sketched in Figure 1. The Figure 2 represents the flow pattern for the fluid impinge on a porous wall

$x = 0$ , satisfying boundary conditions  $u(0, y) = 1, v(0, y) = 0$ . For  $R(x) = x^3 + x^2$ , the streamline pattern in unbounded domain and for the boundary value problem same as for  $R(x) = x^3$  are given in figures (3) and (4), respectively. The streamline pattern for the function  $R(x)$  defined by Eq.(40) for some values of  $C_{18} (\neq 0), C_{19}, C_{20}$  is sketched in figure (5).

## 4. CONCLUSIONS

It is indicated that the equations governing the steady plane motion of an incompressible fluid of variable viscosity for an arbitrary state equation admit an infinite set of solutions for a class of flows characterized by  $y = R(x) + C_1\Psi + C_2$ . Some flow patterns for some forms of the arbitrary function  $R(x)$  are also presented in unbounded and bounded domains.

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**NOMENCLATURE**

$u, v$	–	velocity components.
$x, y$	–	cartesian coordinates.
$p$	–	pressure of fluid.
$\mu$	–	viscosity coefficient.
$T$	–	temperature
$Re$	–	Reynolds number.
$Pr$	–	Prandtl number.
$Ec$	–	Eckert number.
$\Psi$	–	streamfunction.
$E, F, G$	–	coefficients of the fundamental elements.
$W, J$	–	Jacobin of transformation.
$q$	–	speed of the fluid
$\omega$	–	vorticity
$L$	–	energy function.
$\alpha$	–	angle of inclination.
$\Gamma_{11}^2, \Gamma_{12}^2$	–	christopher symbols.
$A, M, R, M_1, \zeta,$ $N, N_1, N_2, N_3,$ $N_4, N_5, N_6, N_7,$ $T_1, T_2, T_3, T_4, Z_1,$ $Z_2, Z_3, X_1, X_2,$ $X_3$	–	functions
superscripts		
$' , '' , ''', V, 1V$	–	differentiation w .r .t. argument.
subscripts		
$x, y$	–	differentiation w .r .t. cartesian coordinates.
$\Psi$	–	differentiation w.r.t $\Psi$ coordinate.



**APPENDIX - A**

$$N_1(x) = T_{1xx} - R'' T_2 / C_1 - 2 R' T_{2x} + 2 (1 + R'^2) T_3 - \text{Re Pr } T_{1x} / C_1 \\ + \text{Ec Pr } R''^2 M / C_1^2$$

$$N_2(x) = T_{2xx} - 2 R'' T_3 - \text{Re Pr } T_{2x} / C_1 + \text{Ec Pr } R''^2 M_1 / C_1^2$$

$$N_3(x) = T_{3xx} - \text{Re Pr } T_{3x} / C_1$$

$$X_1(x) = R'' M'' - 2 R' R'' M_1' + 2 R''' M_1' - [(R' R'')_x + R' R'''] M_1'$$

$$X_2(x) = R'' M_1'' - 4 R' R'' M_2' + 2 R''' M_1' - 2 [(R' R'')_x + R' R'''] M_2' \\ + R^{1V} M_1$$

$$X_3(x) = R'' M_2'' + 2 R''' M_2' + R^{1V} M_2$$

**APPENDIX - B**

$$N_6(x) = T_{1xx} - \text{Re Pr } T_{1x} / C_1 - 2 R' T_{2x} - R'' T_{2x} + 2 (1 + R'^2) T_{3x} \\ + \text{Ec Pr } R''^2 / C_1^2$$

$$N_7(x) = T_{2xx} - \text{Re Pr } T_{2x} / C_1 - 4 R' T_{3x} - 2 R'' T_{3x} \\ + 6 (1 + R'^2) T_{4x} + \text{Ec Pr } R''^2 M_1 / C_1^2$$

$$N_8(x) = T_{3xx} - \text{Re Pr } T_{3x} / C_1 - 6 R' T_{4x} - 3 R'' T_{4x} \\ + \text{Ec Pr } R''^2 M_2 / C_1^2$$

$$N_9(x) = T_{4xx} - \text{Re Pr } T_{4x} / C_1$$